

Appendix C

Historic Plans

C-1 – Excerpts from Final Drainage Report for the Parker 234 Subdivision

C-2 – Chambers and Hess Filing No. 1 Drainage Map

C-3 – Design Flows for EX-1 (A-12)

The developed site can be divided into four (4) major basins, being Basins A, B, C and D. Each of these major basins contains a proposed water quality/ detention pond area.

Basin A

Basin A is comprised of most of the eastern portion of the project, including the proposed commercial site, and contributes runoff to Pond A. This facility is located in the northeasterly corner of the site, adjacent to and immediately west of the southerly extension of Jordan Rd. Pond A will discharge easterly, under Jordan Road, to the existing drainageway to Cherry Creek. Basin A is subdivided into thirteen sub-basins, and generally corresponds to historic basins C-3, C-4, C-5 and a portion of historic basin C-2. Runoff within Basin A flows overland to the internal storm drainage system, and ultimately in Pond A.

The proposed detention pond for Basin A serves only the residential portion. At such time that the commercial lot is developed, a separate detention and water quality facility will need to be provided to service that area.

Pond A is located in Tract B. Storm water will be directed to this pond via overland flow and Storm Drain Line B. The pond is sized to hold the required volume for 100-year detention and water quality per the Town of Parker and UDFCD requirements. This needed 100 year volume is 2.72. The water quality volume required is 0.68 Ac.ft. The total volume, including 100-year detention and WQCV, is accumulated by elevation 5992.1. The weir structure will have a top elevation at 5995.0 and a bottom equal to the 100-year water surface elevation, 5992.1. A 1.42' diameter orifice plate will be installed on the outlet pipe to control to pond's allowable release rate, 36.39 cfs. An outlet pipe is sized to convey 100% of the tributary developed 100-year flow, $Q_{100yr.} = 191.70$ cfs. Storm events that exceed the volume provided in Pond A will be routed through the pond by the emergency overflow spillway. Both pond exits, the spillway and the storm drain, will be protected by riprap.

During initial and interim construction phases, Pond A will have a temporary riser pipe, rather than the permanent outlet structure to allow it to function as a sediment control pond. Also, the spillway will not be cut out of the earth berm that surrounds the pond, so that the pond can have additional volume, which may be needed during the construction operations that typically produce additional sediment. During the final stages of construction, the pond will be modified to include the earth-weir. The perforated outlet pipe will be replaced by the concrete outlet structure.

Basin B

Basin B includes the north-central portion of the project, and directs runoff to detention Pond B. This facility is located adjacent to and immediately southwesterly of the proposed alignment of Chambers Road. Discharge of the computed release rate from Pond B will travel under Chambers Road via a 42" RCP (Storm Line U), into the existing natural drainage-way at that location. The Antelope Heights project, immediately downstream from this discharge point, is coordinating engineering design to accommodate this historic runoff rate. Eventually, this pipe will be connected to the



Project Name/Number Parker 234 / 01804102
Prepared By MEF Date 2-3-03
Sheet 1 of 5

Telephone Log
Meeting Record
Calculations
Other

Divide Basin A

 into Commercial
 & Residential

Commercial Property

developed

12.56 Ac. 95% impervious

$$\rightarrow \text{detention vol.}_{100} = 1.852 \text{ Ac. ft.}$$

$$\text{WQ CV} = \frac{0.562 \text{ Ac. ft.}}{2.414 \text{ Ac. ft.}}$$

Residential Property

30.25 Ac. 56% impervious

$$\rightarrow \text{detention vol.}_{100} = 2.718 \text{ Ac. ft.}$$

$$\text{WQ CV} = \frac{0.676 \text{ Ac. ft.}}{3.394 \text{ Ac. ft.}}$$

$$= 147,843 \text{ ft}^3$$



CONSULTANTS, INC.
 CIVIL ENGINEERING
 LAND SURVEYING
 LAND PLANNING

Project Name/Number Parkway 234 / 01804102
 Date: 2-3-03
 Sheet 2 of 5

Telephone Log
 Meeting Record
 Calculations
 Other

<u>POND A</u>											
Area = 30.25 Ac.											
# of homes = 130 avg. sq. footage = 1660 ft ² , 2 story											
Area (park) = 1.71 Ac.											
Area (lots) = 15.46 Ac.											
Area (roads) = 11.19 Ac.											
Area (open space) = 4.05 Ac.											
130 / 15.46 = 8.41 dwellings / Ac. → 36% impervious per R0-5											
$\frac{1.71(5\%) + 15.46(36\%) + 11.19(100\%) + 4.05(0\%)}{30.25 \text{ Ac.}} = 56\%$											

Detention (V=KA)

DETENTION REQUIREMENTS - ONSITE BASINS

Subdivision: Parker 234
 Location: Parker

Project Name: Parker 234
 Project No. 1804102
 By: MEF
 Checked By: KAL
 Date: 01/24/03

SOIL GROUPS B/C

Q10R= 0.23
 Q100R= 0.85

Note: Allowable release rates for type C soil groups is greater than type B soils, however, rates for type B soil was used for conservatism.

BASIN/LAND USE	DRAINAGE AREA (AC.)	% IMPERV.	V ₁₀ (AC. FT.)	V ₁₀₀ (AC. FT.)	Q _{10R} (CFS)	Q _{100R} (CFS)
Basin A	30.25	56	1.552	2.718	6.96	25.71
Basin B	59.88	54	2.958	5.193	13.77	50.90
Basin C	8.50	25	0.186	0.337	1.96	7.23
Basin D	34.41	26	0.785	1.423	7.91	29.25
Commerical Property	12.6	95	1.110	1.852	2.89	10.68
SUM			6.590	11.524	33.5	123.8

DETENTION PONDING FORMULAS:

$$V_{100} = K_{100} \times A$$

$$V_{10} = K_{10} \times A$$

$$K_{100} = (1.78I - 0.002I^2 - 3.56) / 1000$$

$$K_{10} = (0.95I - 1.90) / 1000$$

$$Q_{100R} = Q_{100R} \times A$$

$$Q_{10R} = Q_{10R} \times A$$

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

Sheet 1 of 3

Designer: MEF
 Company: CVL Consultants
 Date: January 31, 2003
 Project: Parker 234
 Location: Pond A

<p>1. Basin Storage Volume</p> <p>A) Tributary Area's Imperviousness Ratio ($i = I_a / 100$)</p> <p>B) Contributing Watershed Area (Area)</p> <p>C) Water Quality Capture Volume (WQCV) ($WQCV = 1.0 * (0.91 * I^3 - 1.19 * I^2 + 0.78 * I)$)</p> <p>D) Design Volume: $Vol = (WQCV / 12) * Area * 1.2$</p>	<p>$I_a =$ <u>56.00</u> % $i =$ <u>0.56</u></p> <p>Area = <u>30.25</u> acres</p> <p>WQCV = <u>0.22</u> watershed inches</p> <p>Vol = <u>0.676</u> acre-feet</p>
<p>2. Outlet Works</p> <p>A) Outlet Type (Check One)</p> <p>B) Depth at Outlet Above Lowest Perforation (H)</p> <p>C) Required Maximum Outlet Area per Row, (A_o)</p> <p>D) Perforation Dimensions (enter one only): i) Circular Perforation Diameter OR ii) 2" Height Rectangular Perforation Width</p> <p>E) Number of Columns (nc, See Table 6a-1 For Maximum)</p> <p>F) Actual Design Outlet Area per Row (A_o)</p> <p>G) Number of Rows (nr)</p> <p>H) Total Outlet Area (A_{ot})</p>	<p><input checked="" type="checkbox"/> Orifice Plate <input type="checkbox"/> Perforated Riser Pipe <input type="checkbox"/> Other: _____</p> <hr/> <p>H = <u>4.27</u> feet</p> <p>$A_o =$ <u>0.52</u> square inches</p> <p>D = <u>0.813</u> inches, OR W = _____ inches</p> <p>nc = <u>1</u> number</p> <p>$A_o =$ <u>0.52</u> square inches</p> <p>nr = <u>13</u> number</p> <p>$A_{ot} =$ <u>6.65</u> square inches</p>
<p>3. Trash Rack</p> <p>A) Needed Open Area: $A_r = 0.5 * (\text{Figure 7 Value}) * A_{ot}$</p> <p>B) Type of Outlet Opening (Check One)</p> <p>C) For 2", or Smaller, Round Opening (Ref.: Figure 6a): i) Width of Trash Rack and Concrete Opening (W_{conc}) from Table 6a-1 ii) Height of Trash Rack Screen (H_{TR})</p>	<p>$A_r =$ <u>231</u> square inches</p> <p><input checked="" type="checkbox"/> \leq 2" Diameter Round <input type="checkbox"/> 2" High Rectangular <input type="checkbox"/> Other: _____</p> <hr/> <p>$W_{conc} =$ <u>6</u> inches</p> <p>$H_{TR} =$ <u>81</u> inches</p>

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

Sheet 2 of 3

Designer: MEF
Company: CVL Consultants
Date: January 31, 2003
Project: Parker 234
Location: Pond A

<p>iii) Type of Screen (Based on Depth H), Describe if "Other"</p> <p>iv) Screen Opening Slot Dimension, Describe if "Other"</p> <p>v) Spacing of Support Rod (O.C.) Type and Size of Support Rod (Ref.: Table 6a-2)</p> <p>vi) Type and Size of Holding Frame (Ref.: Table 6a-2)</p> <p>D) For 2' High Rectangular Opening (Refer to Figure 6b):</p> <p>i) Width of Rectangular Opening (W)</p> <p>ii) Width of Perforated Plate Opening ($W_{conc} = W + 12"$)</p> <p>iii) Width of Trashrack Opening ($W_{opening}$) from Table 6b-1</p> <p>iv) Height of Trash Rack Screen (H_{TR})</p> <p>v) Type of Screen (based on depth H) (Describe if "Other")</p> <p>vi) Cross-bar Spacing (Based on Table 6b-1, KlempTM KPP Grating). Describe if "Other"</p> <p>vii) Minimum Bearing Bar Size (KlempTM Series, Table 6b-2) (Based on depth of WQCV surcharge)</p>	<p><u> x </u> S.S. #93 VEE Wire (US Filter) Other: _____</p> <hr/> <p><u> X </u> 0.139" (US Filter) Other: _____</p> <hr/> <p><u> 0.75 </u> inches #156 VEE</p> <hr/> <p>3/8 in. x 1.0 in. flat bar</p> <hr/> <p>W = <u> </u> inches $W_{conc} =$ <u> </u> inches $W_{opening} =$ <u> </u> inches $H_{TR} =$ <u> </u> inches</p> <p><u> </u> KlempTM KPP Series Aluminum Other: _____</p> <hr/> <p><u> </u> inches Other: _____</p> <hr/>
<p>4. Detention Basin length to width ratio</p>	<p><u> 1.00 </u> (L/W)</p>
<p>5 Pre-sedimentation Forebay Basin - Enter design values</p> <p>A) Volume (no less than 5% of Design Volume from 1D)</p> <p>B) Surface Area</p> <p>C) Connector Pipe Diameter (Size to drain this volume in 5-minutes under inlet control)</p> <p>D) Paved/Hard Bottom and Sides</p>	<p><u> 0.062 </u> acre-feet</p> <p><u> 0.067 </u> acres</p> <p><u> 6 </u> inches</p> <p><u> y </u> yes/no</p>

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

Designer: MEF
Company: CVL Consultants
Date: January 31, 2003
Project: Parker 234
Location: Pond A

<p>6. Two-Stage Design - See Figure EDB-1</p> <p>A) Top Stage (Depth $D_{WQ} = 2'$ Minimum)</p> <p>B) Bottom Stage Depth ($D_{BS} = 1.0'$ Minimum, $2.0'$ Maximum) Bottom Stage Storage (no less than 3% of Design Volume (0.02027596032 acre-feet.))</p> <p>C) Micro Pool (Minimum Depth = the Larger of 0.5 * Top Stage Depth (1.3') or 2.5')</p> <p>D) Total Volume: $Vol_{tot} = \text{Storage from 5A} + 6A + 6B$ (Must be > Design Volume in 1D, or 0.675865344 acre-feet.)</p>	<p>$D_{WQ} = \underline{2.60}$ feet Storage = $\underline{0.645}$ acre-feet</p> <p>$D_{BS} = \underline{1.50}$ feet Storage = $\underline{0.031}$ acre-feet Surf. Area = $\underline{0.021}$ acres</p> <p>Depth = $\underline{2.50}$ feet Storage = $\underline{0.024}$ acre-feet Surf. Area = $\underline{0.010}$ acres</p> <p>$Vol_{tot} = \underline{0.738}$ acre-feet</p>
<p>7. Basin Side Slopes (Z, horizontal distance per unit vertical) Minimum Z = 4, Flatter Preferred</p>	<p>Z = $\underline{4.00}$ (horizontal/vertical)</p>
<p>8. Dam Embankment Side Slopes (Z, horizontal distance) per unit vertical) Minimum Z = 3, Flatter Preferred</p>	<p>Z = $\underline{4.00}$ (horizontal/vertical)</p>
<p>9. Vegetation (Check the method or describe "Other")</p>	<p><input checked="" type="checkbox"/> Native Grass <input type="checkbox"/> Irrigated Turf Grass Other: _____</p>

Notes: _____

Pond Volume (FAA Method)

Subdivision Parker 234
 Location Parker

Project Name: Parker 234
 Project No. 1804102

By: MEF

Checked By: KAL

Date: 1/31/03

Volume= $\frac{1}{3} \times \text{Depth} \times (A+B+(A*B)^{0.5})$

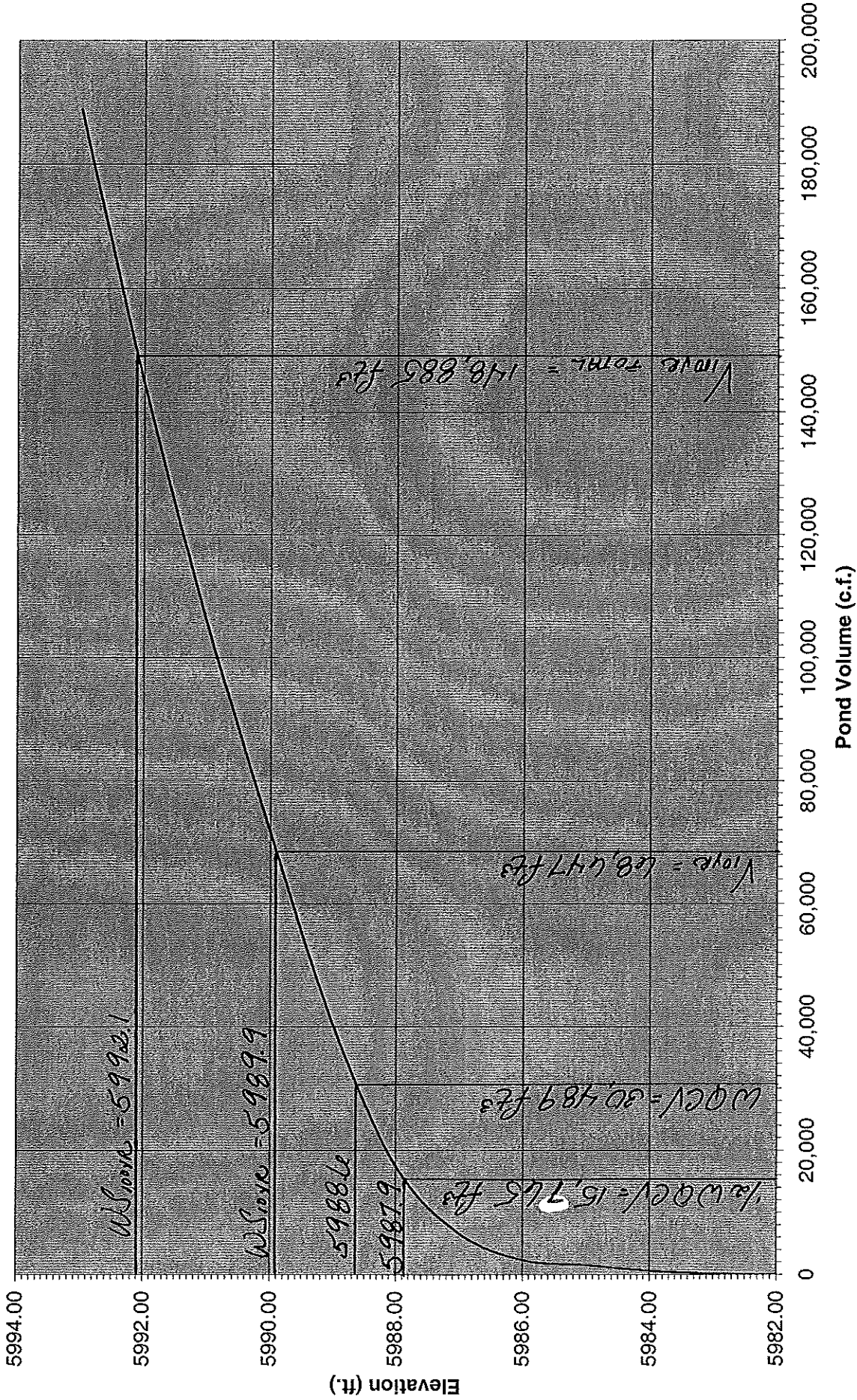
A - Upper Surface

B - Lower Surface

Pond A

Elevation	Surface Area (square feet)	$A+B+(A*B)^{0.5}$	1/3	Depth (feet)	Volume (cubic feet)	Cumulative Volume (cubic feet)
5982.00	0	0.0	0.0	0.00	0	0
5983.00	301	301.0	100.3	1.00	100	100
5984.00	751	1527.4	509.1	1.00	509	609
5984.50	984	2594.6	864.9	0.50	432	1,042
5985.00	1,332	3083.2	1027.7	0.50	514	1,556
5986.00	2,485	2485.0	828.3	1.00	828	2,384
5987.00	6,297	12737.8	4245.9	1.00	4,246	6,630
5988.00	16,152	32534.1	10844.7	1.00	10,845	17,475
5989.00	29,981	68138.8	22712.9	1.00	22,713	40,188
5990.00	32,693	93981.6	31327.2	1.00	31,327	71,515
5991.00	35,507	102271.0	34090.3	1.00	34,090	105,605
5992.00	42,544	116917.6	38972.5	1.00	38,973	144,578
5993.00	46,080	132900.7	44300.2	1.00	44,300	188,878

Pond A Stage-Storage



Emergency Spillway Weir Calculations

Project Name: Parker 234
Project No. 1804102
Calculated By: MEF
Checked By: KAL
Date: 1/31/03

Weir Equation:

$$Q = C * L * (H)^{3/2}$$

$C_d = 3.37$ (trapezoidal weirs)

Note: Weirs are designed to pass 2x the 100yr. tributary flow.
(Refer to SF-3 form)

Pond A Emergency Spillway

Flow Rate (2*Q₁₀₀) = 383.4 cfs
Top of Berm Elevation = 5995.00 feet Freeboard = 1.00
Emergency Spillway Elevation = 5994.00 feet
100 yr. Water Surface Elevation = 5992.10 feet
Height (H) = 1.90 feet
Length (D) = 43.48 feet

Pond B Emergency Spillway

Flow Rate (2*Q₁₀₀) = 353.1 cfs
Top of Berm Elevation = 6089.00 feet Freeboard = 1.00
Emergency Spillway Elevation = 6088.00 feet
Bottom of Berm Elevation* = 6086.00 feet *100 yr. W.S. Elevation = 6083.8 feet
Height (H) = 2.00 feet
Length (D) = 37.08 feet

Pond C Emergency Spillway

Flow Rate (2*Q₁₀₀) = 58.1 cfs
Top of Berm Elevation = 6118.00 feet Freeboard = 1.00
Emergency Spillway Elevation = 6117.00 feet
100 yr. Water Surface Elevation = 6116.20 feet
Height (H) = 0.80 feet
Length (D) = 24.13 feet

Pond D Emergency Spillway

Flow Rate (2*Q₁₀₀) = 160.0 cfs
Top of Berm Elevation = 6050.50 feet Freeboard = 1.00
Emergency Spillway Elevation = 6049.50 feet
100 yr. Water Surface Elevation = 6048.50 feet
Height (H) = 1.00 feet
Length (D) = 47.53 feet

Circular Orifice Sizing

Pond A

DATA:

Flow Rate (Q) = 25.71 cfs
 Water Surface Elevation = 5992.10 feet
 Invert of Orifice = 5981.80 feet
 Height of water surface = 10.30 feet
 to invert of orifice (Y)
 Diameter of Orifice (D) = 1.42 feet
 Height of water surface = 10.30 feet
 to centroid of orifice (h)
 $C_d = 0.65$ for circular orifices
 $g = 32.20 \text{ ft/s}^2$

Project Name: Parker 234
 Project No. 1804102
 Calculated By: MEF
 Checked By: KAL
 Date: 01/31/03

Orifice Equation:

$$Q = C_d * A * (2gh)^{1/2}$$

$$Q = C_d * 3.1415 * D^2 / 4 * (2gh)^{1/2}$$

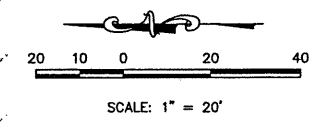
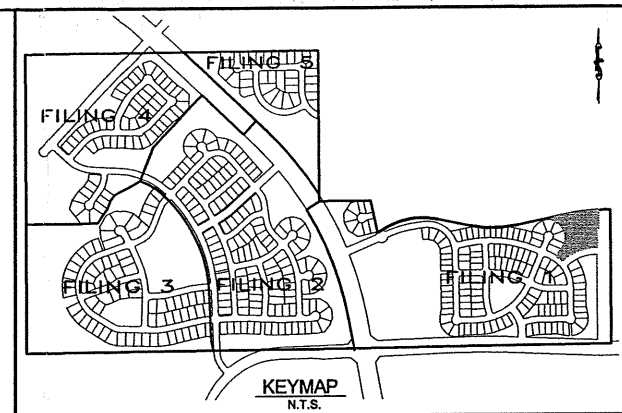
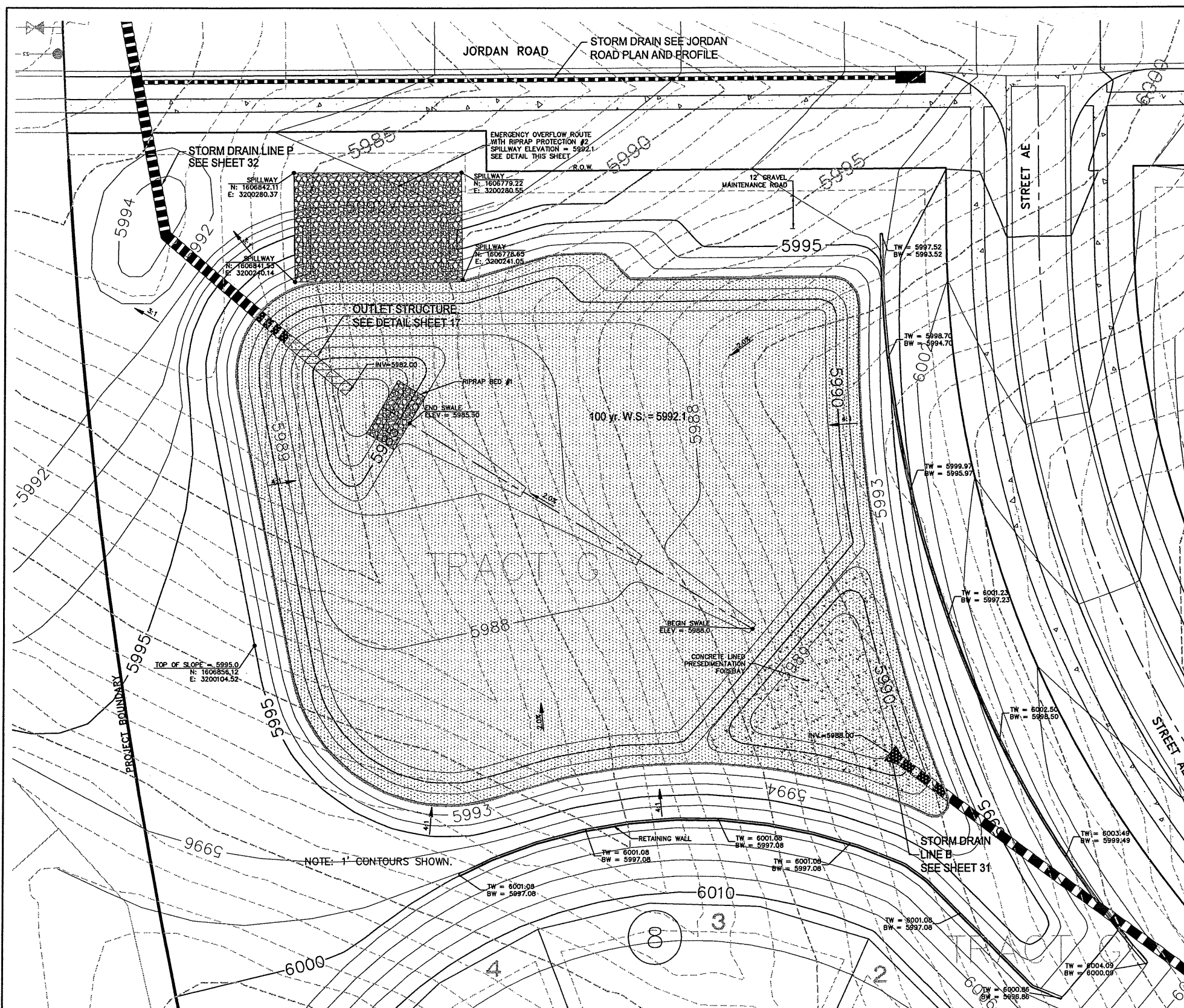
$$Q = 0.65 * 3.1415 * D^2 / 4 * (2 * 32.2 * h)^{1/2}$$

$$D = (Q / (.5105 * (64.4 * h)^{1/2}))^{1/2}$$

Calculation Table for Orifice Size

%	h = %*Y	Diam. (D)	Actual h	h/Y
98%	10.09	1.41	9.60	93%
97%	9.99	1.41	9.60	93%
96%	9.89	1.41	9.59	93%
95%	9.79	1.42	9.59	93%
94%	9.68	1.42	9.59	93%
93%	9.58	1.42	9.59	93%
92%	9.48	1.43	9.59	93%
91%	9.37	1.43	9.58	93%
90%	9.27	1.44	9.58	93%
89%	9.17	1.44	9.58	93%
88%	9.06	1.44	9.58	93%
87%	8.96	1.45	9.58	93%
86%	8.86	1.45	9.57	93%
85%	8.76	1.46	9.57	93%
84%	8.65	1.46	9.57	93%
83%	8.55	1.47	9.57	93%
82%	8.45	1.47	9.57	93%
81%	8.34	1.47	9.56	93%
80%	8.24	1.48	9.56	93%
79%	8.14	1.48	9.56	93%
78%	8.03	1.49	9.56	93%

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RIRAP SUMMARY TABLE

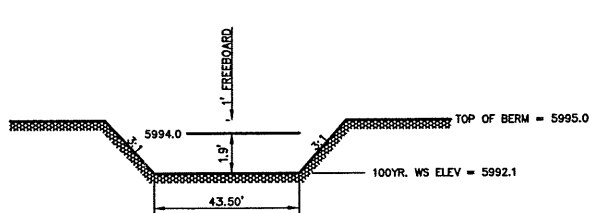
	RR#1	RR#2
LENGTH	23	61'
WIDTH	12	40'
DEPTH	2.5'	1.5'
SIZE d50	9"	12"
TYPE	L	M

* SEE DETAIL

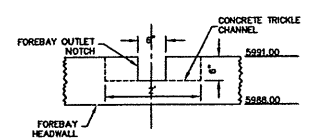
BURY TYPE L RIPRAP WITH 4" NATIVE TOPSOIL AND RESEED OR RESOD.

POND SUMMARY TABLE

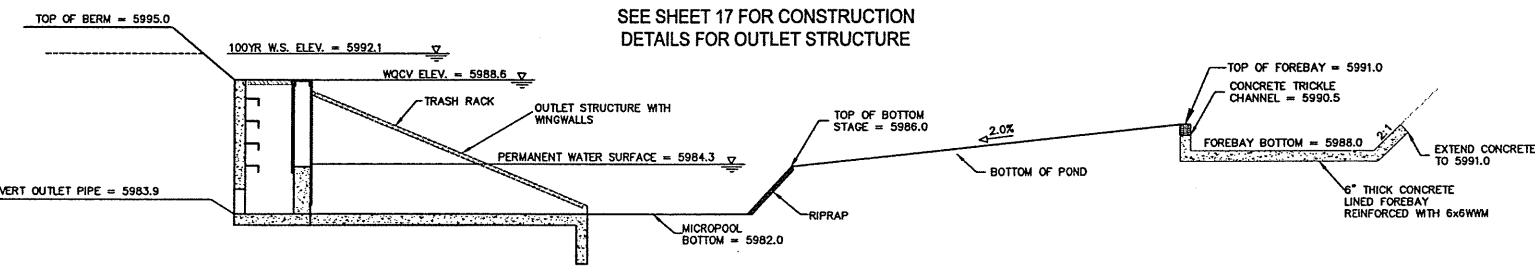
	Q 10yr.	Q 100yr.
PEAK INFLOW (cfs)	127.4	191.7
PEAK OUTFLOW (cfs)	7.0	50.9
WQCV (Ac.Ft.)		0.68
10 yr. REQUIRED VOL. (Ac.Ft.)		1.55
100 yr. REQUIRED VOL. (Ac.Ft.)		2.72
DETENTION CAPACITY (Ac.Ft.)		3.42
AVAILABLE FREEBOARD (ft.)		1.0



EMERGENCY SPILLWAY DETAIL



FOREBAY OUTLET NOTCH



POND A: CROSS SECTION
NOT TO SCALE

Revisions	No.	Date	Init.	Appr.	Date

7901 E. Indianway Avenue
Suite 150
Englewood, CO 80111
Tel: (720) 482-9526
Fax: (720) 482-9546

UNCC
CONSULTANTS OF COLORADO, INC.
CIVIL ENGINEERING - LAND SURVEYING - LAND PLANNING

Continental Homes
7600 East Orchard Road, Ste. 165-S
Greenwood Village, CO 80111

DOUGLAS 234
FILING 1
STREET AND DRAINAGE IMPROVEMENTS
POND A

SCALE: AS SHOWN
FILE NO: 01804102
DATE: FEBRUARY 2003

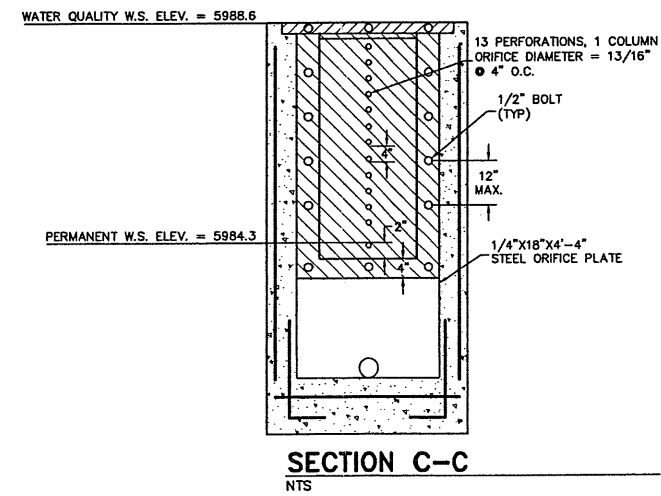
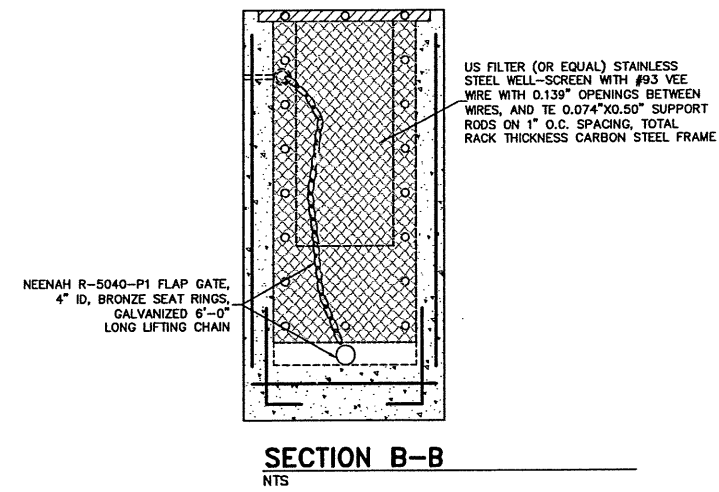
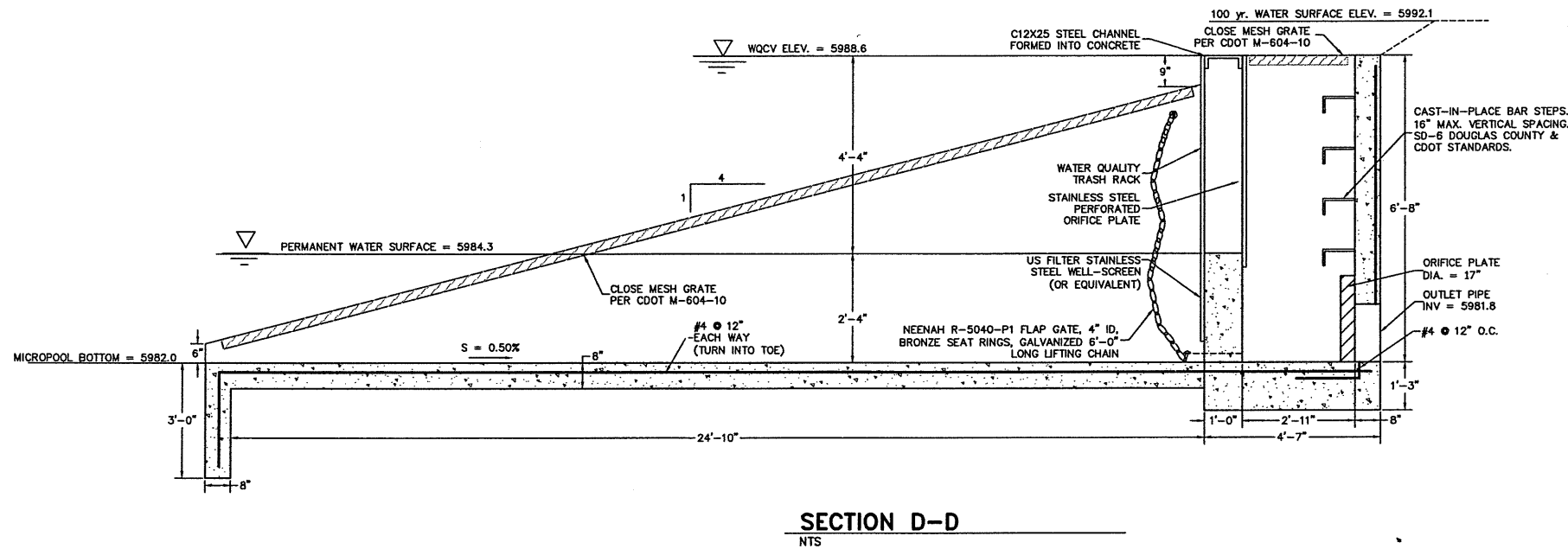
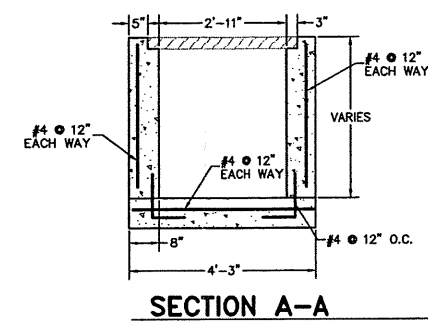
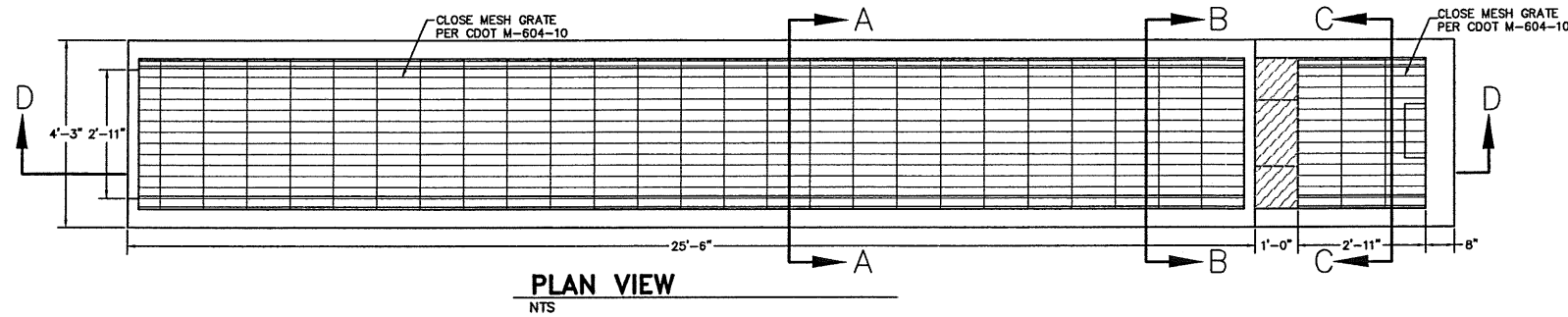
DRAWN BY: JAM
CHECKED BY: KAL
DATE: FEBRUARY 2003

SHEET NUMBER **16**

CALL UNCC
TWO WORKING DAYS
BEFORE YOU DIG
1-800-922-1987
534-6700 METRO DENVER AREA
UTILITY NOTIFICATION CENTER OF COLORADO

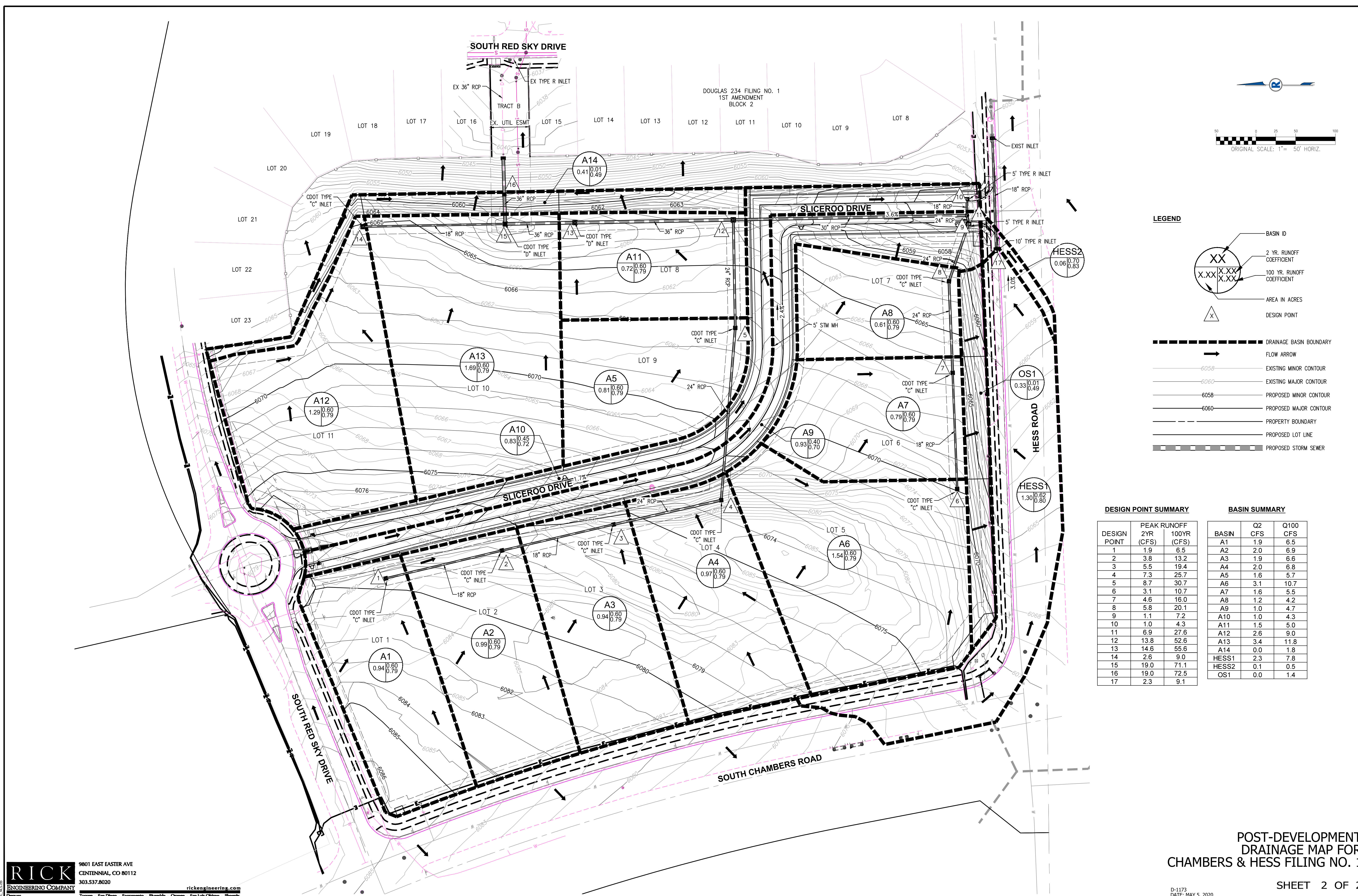
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POND A DETAILS



SHEET NUMBER	DRAWN BY:	SCALE:	FILE NO:	Revisions		Date
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17	MEF	AS SHOWN	01804102			
	KAL					
	DATE:	FEBRUARY 2003				
DOUGLAS 234 FILING 1 STREET AND DRAINAGE IMPROVEMENTS POND A OUTLET DETAILS				Continental Homes 7600 East Orchard Road, Ste. 165-S Greenwood Village, CO 80111		7901 E. Bellevue Avenue Englewood, CO 80111 Tel: (720) 482-9236 Fax: (720) 482-9546 LAND PLANNING CONSULTANTS OF COLORADO, INC. CIVIL ENGINEERING · LAND SURVEYING

DRAWING: 17-PONDA-DET



LEGEND

- XX ○ BASIN ID
- X.XX X.XX ○ 2 YR. RUNOFF COEFFICIENT
- X.XX X.XX ○ 100 YR. RUNOFF COEFFICIENT
- AREA IN ACRES
- △ X △ DESIGN POINT
- DRAINAGE BASIN BOUNDARY
- FLOW ARROW
- 6058 EXISTING MINOR CONTOUR
- 6060 EXISTING MAJOR CONTOUR
- 6058 PROPOSED MINOR CONTOUR
- 6060 PROPOSED MAJOR CONTOUR
- PROPERTY BOUNDARY
- PROPOSED LOT LINE
- PROPOSED STORM SEWER

DESIGN POINT SUMMARY

DESIGN POINT	PEAK RUNOFF 2YR (CFS)	100YR (CFS)
1	1.9	6.5
2	3.8	13.2
3	5.5	19.4
4	7.3	25.7
5	8.7	30.7
6	3.1	10.7
7	4.6	16.0
8	5.8	20.1
9	1.1	7.2
10	1.0	4.3
11	6.9	27.6
12	13.8	52.6
13	14.6	55.6
14	2.6	9.0
15	19.0	71.1
16	19.0	72.5
17	2.3	9.1

BASIN SUMMARY

BASIN	Q2 CFS	Q100 CFS
A1	1.9	6.5
A2	2.0	6.9
A3	1.9	6.6
A4	2.0	6.8
A5	1.6	5.7
A6	3.1	10.7
A7	1.6	5.5
A8	1.2	4.2
A9	1.0	4.7
A10	1.0	4.3
A11	1.5	5.0
A12	2.6	9.0
A13	3.4	11.8
A14	0.0	1.8
HESS1	2.3	7.8
HESS2	0.1	0.5
OS1	0.0	1.4

RICK ENGINEERING COMPANY
 9801 EAST EASTER AVE
 CENTENNIAL, CO 80112
 303.537.8020
 rickengineering.com

D-1173
 DATE: MAY 5, 2020

SHEET 2 OF 2

NOT FOR CONSTRUCTION – EXHIBIT FOR DRAINAGE STUDY REPORT ONLY

**STANDARD FORM SF-3
STORM DRAINAGE SYSTEM DESIGN
(RATIONAL METHOD PROCEDURE)**

CALCULATED BY:
DATE:
CHECKED BY:

BHE
5/4/20

P1= 2.60

JOB NO: D01173
PROJECT: CHAMBERS AND HESS FILING NO. 1
DESIGN STORM: 100 YEAR

BASIN	DESIGN POINT	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		AREA DESIG.	AREA (Acres)	RUNOFF COEFF	Tc (min)	C A (Acres)	I (in/hour)	Q (cfs)	Tc (min)	(C A) (Acres)	I (in/hour)	Q (cfs)	SLOPE (%)	STREET FLOW (cfs)	DESIGN FLOW (cfs)	SLOPE (%)	PIPE SIZE (in)	LENGTH (ft)	VELOCITY (fps)	Tt (min)	
A1	1	A1	0.94	0.79	5.0	0.74	8.82	6.5							6.5	1.2	18	147	6.7	0.4	INL-09 TO INL-08
A2	2		0.99	0.79	5.0	0.78	8.82	6.9													
	2	A1+A2							5.4	1.53	8.65	13.2			13.2	1.8	18	141	9.0	0.3	INL-08 TO INL-07
A3	3		0.94	0.79	5.0	0.75	8.82	6.6													
	3	A1-A3							5.6	2.27	8.54	19.4			19.4	3.2	24	137	12.6	0.2	INL-07 TO INL-06
A4	4		0.97	0.79	5.0	0.77	8.82	6.8													
	4	A1-A4							5.8	3.04	8.46	25.7			25.7	1.8	24	218	10.8	0.3	INL-06 TO INL-05
A5	5		0.81	0.79	5.0	0.64	8.82	5.7													
	5	A1-A5							6.1	3.68	8.32	30.7			30.7	10.5	24	136	22.3	0.1	INL-05 TO SDMH-01
A6	6	A6	1.54	0.79	5.0	1.22	8.82	10.7						10.7	3.0	18	146	10.6	0.2	INL-14 TO INL-13	
A7	7	A6-A7	0.79	0.79	5.0	0.62	8.82	5.5	5.2	1.84	8.71	16.0			16.0	6.3	24	115	15.4	0.1	INL-13 TO INL-12
A8	8	A6-A8	0.61	0.79	5.0	0.48	8.82	4.2	5.4	2.32	8.66	20.1			20.1	5.0	24	76	15.0	0.1	INL-12 TO INL-11
OS1			0.33	0.49	5.0	0.16	8.82	1.4													
HESS1	17	HESS1	1.30	0.80	8.4	1.04	7.52	7.8	8.4	1.21	7.52	9.1									
									8.4	0.84	7.52	6.3									
									8.4	0.37	7.52	2.8									CAPTURED BY INLET INL-15 BYPASSED INLET 15 TO INLET A11
HESS2			0.06	0.83	5.0	0.05	8.82	0.5													
A9	9	A9+HESS1+HESS2	0.93	0.70	9.1	0.65	7.29	4.7	9.1	1.07	7.29	7.8									INL-11 INLET DESIGN
		A6-A9+HESS1+HESS2							9.1	3.39	7.29	24.7			24.7	0.5	24	11	7.9	0.0	DP9: RUNOFF LEAVING INL-11
A10	10	A10	0.83	0.72	9.8	0.60	7.10	4.3						4.3	0.5	18	21	4.4	0.1	INL-10 TO SDMH-02	
	11	A6-A10							9.9	3.99	7.07	28.2			28.2	0.5	24	294	9.0	0.5	SDMH-02 TO SDMH-01
	12	A1-A10							10.4	7.67	6.92	53.1			53.1	0.5	36	199	7.5	0.4	SDMH-01 TO INL-04
A11	13	A1-A11	0.72	0.79	5.0	0.57	8.82	5.0	10.8	8.24	6.81	56.1			56.1	0.5	36	88	7.9	0.2	INL-04 TO INL-02
A12	14	A12	1.29	0.79	5.0	1.02	8.82	9.0						9.0	8.1	18	179	14.6	0.2	INL-03 TO INL-02	

Proposed flow is 8.8 cfs



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